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# Non-linear Detached-Eddy Simulations on Supercomputing Facilities

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## Introduction



- 2 Scalability Tests Lid–driven cavity
- **4** Conclusions



- The long term goal of this research work is to develop a CFD approach to investigate accurately and efficiently (as more as possibile) fluid flow phenomena involving wakes, such as:
  - Wind turbines
  - Pin fin arrays

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- $\bullet$  Provide a contribution to the ongoing search for a better hybrid LES/RANS approach applicable to high  ${\rm Re}$  flows. In particular:
  - a quadratic constitutive relation (QCR) for Reynolds Stresses introduced in [Spalart, 2000] for RANS equations is here evaluated in SA-DES environment
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  - a standard SA–DES computation was also performed
- Perform scalability tets for OpenFOAM code on the GALILEO supercomputing facility (just installed at CINECA)

# Scalabilty tests

Strong scalability tests have been conducted on GALILEO supercomputing facility @CINECA considering the following parameters:

- Total number of cells
- Linear-solvers
- Compiler/MPI implementation effect
  - GNU compilers + Open MPI (built with GNU compilers)
  - $Intel^{\mathbb{R}}compilers + Intel^{\mathbb{R}}MPI$  library
  - Intel<sup>®</sup> compilers + Open MPI (built with Intel<sup>®</sup> compilers)
  - Intel<sup>®</sup> compilers + Open MPI (built with GNU compilers)

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### Lid-driven cavity flow



Streamlines, [Vratis Ltd, 2015]

- Cubic domain, H = 1, Re = 10;
- icoFoam solver;
- Structured uniformly spaced grid;
- 40 time-steps without I/O as in [Culpo, 2011];
- $\Delta t = 10^{-4};$
- Default linear-solvers:
  - PCG for *p* with DIC preconditioner;
  - smoothSolver for u (symGaussSeidel);
  - PISO correctors: 2;
- Default tollerances:  $p: 10^{-6}$ , **u**:  $10^{-5}$ .

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### Grid cells



Figure: Effect of different total number of grid cells

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### Grid cells



Figure: Effect of different total number of grid cells

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# **Compilers and MPI implementation**



Figure: Effect of different compilers and MPI implementations (2 · 10<sup>6</sup> cells)

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## **Compilers and MPI implementation**



Figure: Effect of different compilers and MPI implementations (2 · 10<sup>6</sup> cells)

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### Linear solvers

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smoothSolver for u (symGaussSeidel);
PISO correctors: 2.

р

solver	GAMG;
tolerance	1e-06;
relTol	0;
smoother	GaussSeidel;
nPreSweeps	0;
nPostSweeps	2;
nFinestSweeps	2;
cacheAgglomerat	ion on;
agglomerator	<pre>faceAreaPair;</pre>
nCellsInCoarses	tLevel 16-512;
mergeLevels	1;

}

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### Linear solvers



Figure:  $2 \cdot 10^6$  cells

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### Linear solvers



Figure:  $2 \cdot 10^6$  cells

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### Linear solvers



Figure:  $4 \cdot 10^6$  cells

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### Linear solvers



Figure:  $4 \cdot 10^6$  cells

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DES computations		

## **DES** equations

$$\nabla \cdot \mathbf{u} = 0,$$
  

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{u} \otimes \mathbf{u}) = -\frac{1}{\rho} \nabla \rho + \nabla \cdot (2\nu \mathbf{D}) + \nabla \cdot \mathbf{B},$$
  

$$\frac{\partial \tilde{\nu}}{\partial t} + \nabla \cdot (\mathbf{u}\tilde{\nu}) = c_{b1}\tilde{S}\tilde{\nu} + \frac{c_{b2}}{\sigma} \nabla \tilde{\nu} \cdot \nabla \tilde{\nu} + \frac{1}{\sigma} \nabla \cdot ((\nu + \tilde{\nu}) \nabla \tilde{\nu}) - c_{w1} f_w \left(\frac{\tilde{\nu}}{\tilde{d}}\right)^2$$

where:

$$\begin{split} \mathbf{B} &= \mathbf{R} - c_{r1} \left( \mathbf{Q} \cdot \mathbf{R} - \mathbf{R} \cdot \mathbf{Q} \right), \\ \mathbf{R} &= -\frac{2}{3} k \mathbf{I} + 2\nu_t \mathbf{D}, \quad \mathbf{Q} = 2\Omega / \sqrt{\nabla \mathbf{u} : \nabla \mathbf{u}} , \\ \mathbf{D} &= \frac{1}{2} \left( \nabla \mathbf{u} + \nabla \mathbf{u}^T \right), \quad \mathbf{\Omega} = \frac{1}{2} \left( \nabla \mathbf{u} - \nabla \mathbf{u}^T \right), \quad S = \sqrt{2\Omega : \Omega} , \\ \tilde{S} &= S + \frac{\tilde{\nu}}{k^2 d^2} f_{v2}, \quad \nu_t = f_{v1} \tilde{\nu}, \quad \tilde{d} = \min \left( d, C_{DES} \Delta \right). \end{split}$$

# **DES** equations

- $\mathbf{B} = \mathbf{R} c_{r1} \left( \mathbf{Q} \cdot \mathbf{R} \mathbf{R} \cdot \mathbf{Q} \right)$ 
  - it was introduced in [Spalart, 2000] for RANS equations coupled with the one-equation Spalart-Allmaras turbulence model and it allows the prediction of secondary flows
  - it is related related to the proposal of [Wilcox and Rubesin, 1980]
  - this quadratic constitutive relation is considered preliminar in the sense it uses only one of the many possibile combinations of strain rate and rotation tensor
  - $c_{r1} = 0.3$  was obtained in simple boundary layer flows requiring a fair level of anistropy  $\overline{u'u'} > \overline{w'w'} > \overline{v'v'}$
  - it is turbulence model indipendent
- the closure functions and constants of the turbulence/SGS model are standard
- To assess the performance of this constitutive relation in DES envinroment the flow-field around the circular cylinder in subcritical regime ( $\mathrm{Re}=3900$ ) was computed

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## **Computational Grid**



- Structured non-orthogonal grid
- Rectangular domain:
  - 40 D in the wake region
  - 20 D in transverse direction
  - 0.5 D in span-wise direction
- First cell height:  $2 \cdot 10^{-3}D$
- Span-wise direction:  $2 \cdot 10^{-2}D$  uniform spacing
- No wall functions
- No perturbations added at the inlet
- 2.06 · 10<sup>6</sup> cells

# Numerics

- pimpleFOAM solver
- some div-terms:

```
div(phi,U) Gauss linear;
div(phi,nuTilda) Gauss limitedLinear 0.333;
div(nonlinearStress) Gauss linear corrected;
```

- Linear solvers:
  - Preconditioned bi-Conjugate Gradient Method with DILU for  ${\boldsymbol{u}}$
  - Preconditioned bi-Conjugate Gradient Method with DILU for  $\tilde{\nu}$
  - $\bullet\,$  Preconditioned conjugate gradient method with DIC for p
- Tollerances:  $10^{-5}$  for  $p,\,10^{-12}$  for  ${\bf u}$  and  $\tilde{\nu}$
- second order implicit time integration ( $\Delta t = 10^{-3}$ )

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## Parallel performance



Figure: Effect of the linear solver

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### **Vortical structures**





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## 1D energy spectra



	$St_{vs}$
NL-DES	$0.217 \pm 4 \cdot 10^{-3}$
SA–DES	$0.216 \pm 7 \cdot 10^{-3}$
LES-SMAG	0.19
LES-TKE	0.209
Parnaudau	0.208
Ong	0.21

	${\rm St_{vs}/St_{sL}}$
NL-DES	pprox 8.7
SA–DES	pprox 7.3
LES-SMAG	$\approx 8$
LES-TKE	pprox 7
Dong (DNS)	7.83

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### Mean-velocity profiles



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## Mean-velocity profiles



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# $\overline{u'u'}$ profiles



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## $\overline{\mathbf{v}'\mathbf{v}'}$ profiles



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## Aerodynamic forces

	C <sub>I,rms</sub>	C <sub>d,rms</sub>	$\langle C_l \rangle$	$\langle C_d \rangle$
NI –DES	0 3988	1 1 3 7 4	0.0052	1 1 3 7 4
SA-DES	0.3300	1.1077	0.0091	1.1071
LES-SMAG [Lysenko et al., 2012]	0.444	1.19	0.44	1.18
LES-TKE [Lysenko et al., 2012]	0.089	0.97050	0.09	0.97
[Ouvrard et al., 2010] LES	0.092	_	_	0.99
[Meyer et al., 2010] LES	_	_	_	1.05
[Kravchenko and Moin, 2000] LES	_	_	_	1.04
[Mittal and Moin, 1997] LES	_	—	—	1.00
[Franke and Frank, 2002] LES	_	_	_	0.99
[Alkishriwi et al., 2006] LES	_	_	—	1.05
[Mani et al., 2009] LES	_	—	—	0.99
[Wornom et al., 2011] LES	0.11	—	_	0.99
[Lourenco, 1993] PIV	—	—	_	0.99
[Norberg, 1994] HWA	_	_	_	0.98

# Conclusions

- OpenFOAM scalability have been tested on GALILEO with good results.
- NL-DES (using a simple quadratic constitutive relation) and SA-DES97 have been compared in this work. NL-DES seems to be promising (our results are not still full converged).
- Further topics must be addressed:
  - span-wise resolution
  - others constitutive relations
  - DDES/IDDES

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